

# Slurry Impregnation of $\text{ZrO}_2$ Extrudates: Controlled EggShell Distribution of $\text{MoO}_3$ , Hydrodesulfurization Activity, Promotion by Co

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Received: 12 August 2008 / Accepted: 19 September 2008 / Published online: 15 October 2008  
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**Abstract** Catalysts with eggshell/uniform Mo concentration profiles were prepared by a reaction of  $\text{ZrO}_2$  and  $\text{ZrO}(\text{OH})_2$  extrudates with an aqueous slurry of  $\text{MoO}_3$ . The thickness of the shell was regulated by the amount of  $\text{MoO}_3$ .  $\text{CoCO}_3$  was adsorbed onto  $\text{MoO}_3/\text{ZrO}_2$  from its aqueous slurry. The  $\text{ZrO}_2$ -supported catalysts were compared to their  $\text{TiO}_2$ -supported and industrial reference  $\text{Al}_2\text{O}_3$ -supported counterparts in a model reaction of benzothiophene hydrodesulfurization.

**Keywords**  $\text{MoO}_3/\text{ZrO}_2$  · Eggshell Mo catalyst ·  $\text{CoMo}/\text{ZrO}_2$  ·  $\text{CoMo}/\text{TiO}_2$  · Slurry impregnation · Benzothiophene hydrodesulfurization

## 1 Introduction

Catalysts based on  $\text{ZrO}_2$ -supported  $\text{MoO}_3$  exhibit many applications in reactions of industrial importance such as oxidation [1–7], hydrotreating [8–17], metathesis [18], isomerization [19], and water–gas shift [20], in which shaped forms of the catalysts are mostly used. However, the open literature, up to the authors' knowledge, focuses mostly on Mo deposition onto the support grains instead of a shaped form, like extrudates or tablets. In the field of hydrodesulfurization (HDS), only limited effort has been devoted to the impregnation of the most common support,  $\text{Al}_2\text{O}_3$ . The impregnation method using an aqueous solution of  $(\text{NH}_4)_6\text{Mo}_7\text{O}_{24}$  was studied in the works [21–25]. It

was found that lower pH and a higher concentration of the solution, higher temperature, and accelerated drying promoted the formation of a shallow eggshell Mo profile. We, on the other hand, have proposed a new method, called “slurry impregnation” or “water-assisted spreading”, which leads to a sharp and deep Mo eggshell in the  $\text{Al}_2\text{O}_3$  [26] or  $\text{TiO}_2$  [27] extrudates. The method is based on the reaction of  $\text{MoO}_3$  with the extrudates in water, and its main advantage lies in the fact that it does not produce any waste solution, only distilled water, during drying.

Techniques used in the literature [21–27] for the evaluation of Mo profiles in the extrudates or tablets include electron probe micro-analysis (EPMA) and reduction with a hydrazine–hydrochloric solution, with gaseous hydrogen or with a gaseous mixture of hydrogen and hydrogen sulfide. Quite recently, UV-vis and Raman microscopy [28–33], Tomographic Energy Dispersive Diffraction Imaging [34], and Multinuclear Magnetic Resonance Imaging [35] have been proposed as powerful tools for investigation into the preparation of  $\text{Al}_2\text{O}_3$ -supported Co-, Mo-, and P-containing hydrodesulfurization catalysts. It was corroborated that a low pH (5.0) of the impregnation solution resulted in the slow transport of Mo anions into the catalysts because of the strong interaction between these compounds and the support, whereas at high pH (9.0) the interactions were weak and the transport fast. However, at high pH, the drying (calcination) caused a reagglomeration of the poorly-bound Mo species over the external part of the extrudates. This was partially suppressed by the presence of a complexing agent such as citrates, or phosphorus in the Mo impregnation solution [28, 31]. Research [30, 33] into the deposition of Keggin-type complexes  $\text{H}_x\text{P}(\text{MoO}_4)_{11}\text{CoO}_{40}^{(7-x)-}$  has shown that a homogeneous, eggshell or egg yolk distribution of the complex may be obtained by varying the composition of the impregnation solution

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(mainly the P/Mo ratio), aging time and drying procedure. Nonetheless, any impregnated species recrystallizes if the concentration of the compound exceeds the dispersion limits of the support.

The purpose of the work being presented is to report briefly on the deposition of MoO<sub>3</sub> onto ZrO<sub>2</sub> and ZrO(OH)<sub>2</sub> extrudates and of CoCO<sub>3</sub> onto MoO<sub>3</sub>/ZrO<sub>2</sub> catalysts with saturated adsorption loading of MoO<sub>3</sub> while applying the principles of the slurry impregnation method. Since the depositions proceed via adsorption from an aqueous slurry of extremely low-solubility precursors, it is not possible to exceed the dispersion capacity of the supports or the MoO<sub>3</sub>/ZrO<sub>2</sub> catalysts. The process of Mo and Co deposition was monitored visually after reduction sulfidation in a H<sub>2</sub>/H<sub>2</sub>S mixture and by electron probe microanalysis. The activities of the prepared catalysts were determined in their sulfided stage in the model reaction of benzothiophene hydrodesulfurization (HDS) in a laboratory gas-phase fixed-bed reactor. Unfortunately, the internal diameter of the laboratory reactor did not enable us to evaluate the activity of catalysts in the form of extrudates thus only the extrudates with uniform and saturated profile of MoO<sub>3</sub> concentration were tested after crushing to the particle size fraction 0.16–0.32 mm. This approach was, nonetheless, convenient to compare the activity of the prepared ZrO<sub>2</sub>-supported catalysts containing saturated adsorption loadings of MoO<sub>3</sub> and CoO with their TiO<sub>2</sub>-supported counterparts and industrial reference Al<sub>2</sub>O<sub>3</sub>-supported catalysts.

## 2 Experimental

### 2.1 Supports

The ZrO<sub>2</sub> (AlfaAesar, Product No. 43815) extrudates were of an external diameter of 3.2 mm, an average length of 8 mm, a BET surface area of 108 m<sup>2</sup>g<sup>-1</sup>, pore volume of 0.255 cm<sup>3</sup>g<sup>-1</sup> and a BJH average pore diameter of 8.0 nm. The ZrO(OH)<sub>2</sub> (MEL Chemicals, an industrial sample) extrudates with an external diameter of 3 mm and average length of 10 mm contained approximately 15 wt.% of Al<sub>2</sub>O<sub>3</sub> as a binder. Its BET surface area, pore volume and BJH average pore diameter were 311 m<sup>2</sup>g<sup>-1</sup>, 0.166 cm<sup>3</sup>g<sup>-1</sup> and 2.2 nm, respectively.

### 2.2 Preparation of Mo Catalysts

The MoO<sub>3</sub> (Fluka, Product No. 69850) was being ground in a planetary mill for 24 h before use. The mixture consisting of 15 g of support extrudates, 6.43 g of MoO<sub>3</sub>, and 50 mL of H<sub>2</sub>O was being heated under a reflux condenser at 95 °C, with the samples of the six extrudates removed at

various time intervals, subsequently washed with water, dried in a rotary vacuum evaporator at 100 °C, sulfided in a H<sub>2</sub>/H<sub>2</sub>S mixture (see Sect 2.5. for the details of sulfidation), bisected and scanned. Reduction sulfidation changed the MoO<sub>3</sub> from light gray to black without affecting the color of the white-shadow zirconias. At the end of impregnation, the unreacted slurry of MoO<sub>3</sub> was separated from the remaining extrudates by decantation. The resulting saturated extrudates were dried and analyzed for MoO<sub>3</sub> content by atomic absorption spectroscopy (AAS) and designated 7.6MoO<sub>3</sub>/ZrO<sub>2</sub> and 20.8MoO<sub>3</sub>/ZrO(OH)<sub>2</sub>, where 7.6 and 20.8 represented the determined MoO<sub>3</sub> content in wt.%. The 7.6MoO<sub>3</sub>/ZrO<sub>2</sub> extrudates were crushed and sieved to a grain-size fraction of 0.16–0.32 mm so that the HDS activity could be determined. The catalyst 7.6MoO<sub>3</sub>/ZrO<sub>2</sub>(CIM) was prepared by the conventional impregnation method of the support grains with an aqueous solution of (NH<sub>4</sub>)<sub>6</sub>Mo<sub>7</sub>O<sub>24</sub> (vacuum drying of an excess of the impregnation solution) as has been reported elsewhere [17].

Additionally, the ZrO(OH)<sub>2</sub> was allowed to react with the MoO<sub>3</sub>/H<sub>2</sub>O slurry at 25 and 95 °C. Three loadings of MoO<sub>3</sub>, namely 5, 10, and 15 wt.% (calculated per solid part of the mixtures), were used. At the end of the slurry impregnation, all the MoO<sub>3</sub> disappeared from the mixtures and the extrudates were dried in a vacuum evaporator at 100 °C. The actual content of MoO<sub>3</sub> in the final catalysts was analyzed by AAS and was proved to be the same as the nominal one.

The TiO<sub>2</sub>-supported samples 10.5MoO<sub>3</sub>/TiO<sub>2</sub> and 10.5MoO<sub>3</sub>/TiO<sub>2</sub> (CIM) were prepared by slurry impregnation method (spreading of MoO<sub>3</sub> onto TiO<sub>2</sub> in water) and conventional impregnation method (vacuum drying of TiO<sub>2</sub> with an excess of an aqueous solution of (NH<sub>4</sub>)<sub>6</sub>Mo<sub>7</sub>O<sub>24</sub>), respectively. Further details about the synthesis can be found in our earlier work [27].

### 2.3 Preparation of CoMo Catalysts

The mixture of 5 g of MoO<sub>3</sub>/ZrO(OH)<sub>2</sub> extrudates, 0.33 g of CoCO<sub>3</sub> (Aldrich, Product No. 202193, ground in a planetary mill for 24 h) and 18 mL of water was being heated at 95 °C. Samples of extrudates were taken at various time intervals. They were washed with water, dried in a rotary vacuum evaporator at 100 °C, bisected and analyzed with EPMA.

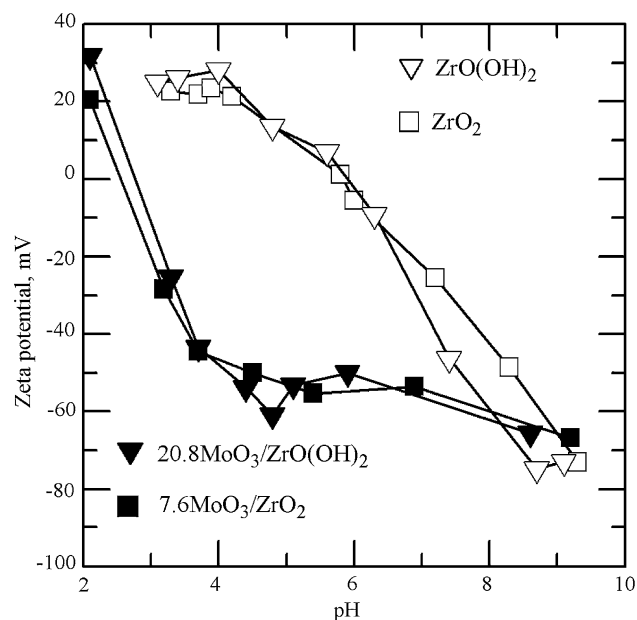
The catalysts 7.6MoO<sub>3</sub>/ZrO<sub>2</sub> and 10.5MoO<sub>3</sub>/TiO<sub>2</sub> in the form of the grain were saturated with Co by their being heated with an aqueous slurry of CoCO<sub>3</sub> under a reflux condenser at 95 °C for 12 h. The nominal loading of Co used for the slurry impregnation corresponded to 5 wt.% of CoO in the final catalysts. The unreacted slurry of CoCO<sub>3</sub> was removed from the grains at the end of impregnation by

washing with water. The actual loading of CoO in wt.% was determined by AAS and the catalysts were labeled: 1.7CoO6.4MoO<sub>3</sub>/ZrO<sub>2</sub> and 2.6CoO10.0MoO<sub>3</sub>/TiO<sub>2</sub>.

Co was also deposited over the 7.6MoO<sub>3</sub>/ZrO<sub>2</sub> and 10.5MoO<sub>3</sub>/TiO<sub>2</sub> catalysts grains by the conventional impregnation method from an aqueous solution of Co(NO<sub>3</sub>)<sub>2</sub> (vacuum drying of an excess of the aqueous impregnation solution) and by impregnation of a pre-sulfided form of those catalysts from a methanolic solution of cobalt-acetylacetonate, Co(C<sub>5</sub>H<sub>7</sub>O<sub>2</sub>)<sub>2</sub>, (vacuum drying of an excess of the methanolic impregnation solution). The catalysts were designated as follows: 2.4CoO(CIM)11.5MoO<sub>3</sub>/TiO<sub>2</sub> and 3.2CoO(MIM)11.1MoS<sub>2</sub>/TiO<sub>2</sub>, where CIM and MIM were used to refer to the Co deposited by the conventional aqueous impregnation method and methanolic impregnation method, respectively. The method of pre-sulfidation is described in Sect 2.5 below.

## 2.4 Characterization of the Materials

The point of zero charge (PZC) was measured by means of a simplified mass titration method [36] with a WTW pH meter equipped with a cell Hamilton Slimtrode. The PZC of the selected samples was also obtained from a plot of zeta potential versus pH, an example of which is given in Fig. 1. The zeta potential was measured with a Coulter Delsa 440 SX (Coulter Electronic, USA). Prior to the measurement, the pH of each sample (0.04 g of solid sample and 40 mL of water) was adjusted with NaOH or HCl.



**Fig. 1** Examples of the dependence of the zeta potential on the pH determined over the zirconias and the catalysts with saturated adsorption loading of MoO<sub>3</sub>

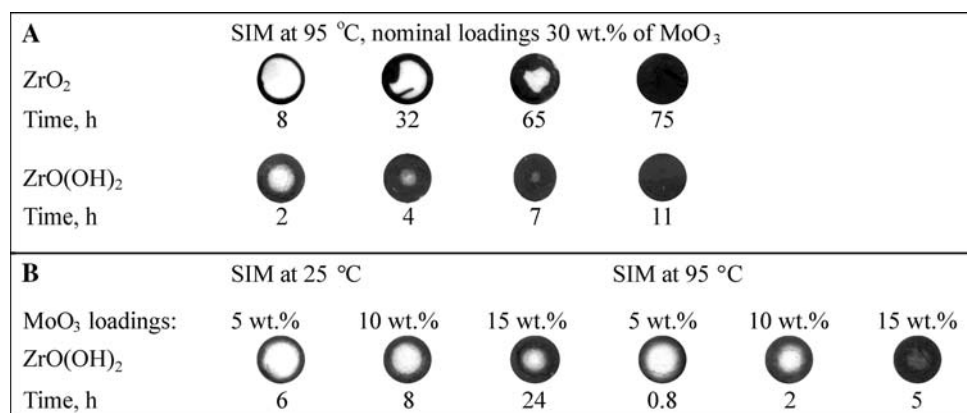
The specific surface area was determined by the common Brunauer, Emmett, and Teller (BET) procedure using a Micromeritics ASAP 2010M instrument after evacuating of the samples at 350 °C for 4 h. The average pore diameter was acquired from the desorption branch of the adsorption-desorption isotherms by the Barrett-Joyner-Halenda (BJH) method.

The Co and Mo content in the saturated catalysts were analyzed by atomic adsorption spectroscopy (AAS) with GBC Avanta instrument. Bisected catalyst extrudates were analyzed using electron probe micro-analysis (EPMA). A JEOL JXA electron microscope was equipped with the ED analyzer EDAX PV 9400. Each point of Co loading represents an average recorded and calculated over the area 60 × 60 μm at a given distance from the extrudates' centers.

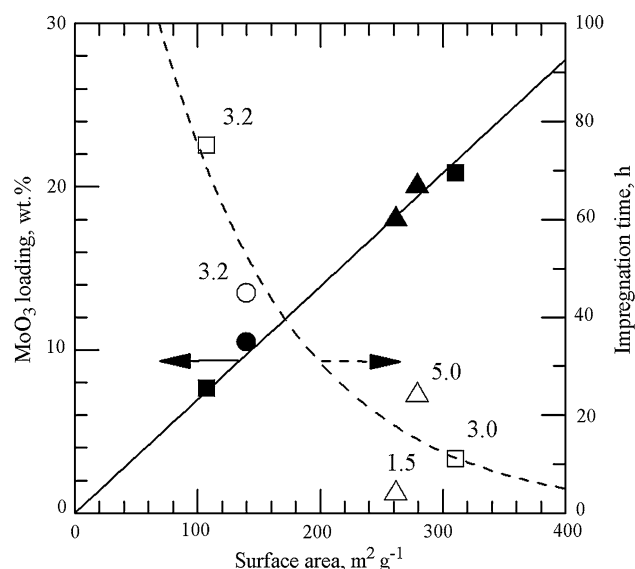
## 2.5 Benzothiophene Hydrodesulfurization

Benzothiophene (BT) hydrodesulfurization (HDS) was carried out in the gas-phase in a fixed-bed tubular-flow microreactor (i.d. 3 mm). The catalysts were presulfided in a H<sub>2</sub>S/H<sub>2</sub> flow (1/10) at a temperature ramp 10 °C min<sup>-1</sup> to 400 °C and a dwell time of 1 h. The composition of the starting reaction mixture was kept constant; namely, the mixture contained 16,200 and 1,384 kPa of BT, decane and hydrogen, respectively. The catalyst charge (W) was varied from 0.02 to 0.4 g, depending on its activity, and was diluted with inert α-Al<sub>2</sub>O<sub>3</sub> to form a bed of a length of 30 mm. The particle size fraction 0.16–0.32 mm of the catalysts and α-Al<sub>2</sub>O<sub>3</sub> diluent was used for the experiments. Over the reference CoMo catalyst KF, it was checked that this particle size fractions exhibited the same activity as lower fraction 0.08–0.16 mm so the influence of internal diffusion was eliminated. The reaction was run at 360 °C and at three feed rates of BT: 7.7, 10.3 and 15.5 mmolh<sup>-1</sup>. The steady state was reached 20 min after each feed-rate change, with no deactivation of the catalysts observed. The reaction mixture was analyzed on a Hewlett-Packard gas chromatograph (6890 series) equipped with a capillary column HP-5 (30 m, 0.53 mm, 1.5 μm) and flame ionization detector. The reaction products were dihydrobenzothiophene (DHBT) and ethylbenzene (EB). The following parameters were determined: (i) the relative composition of the reaction mixture,  $a_i$ , ( $a_{BT} = n_{BT}/n_{BT}^0$ ,  $a_{DHBT} = n_{DHBT}/n_{BT}^0$ ,  $a_{EB} = n_{EB}/n_{BT}^0$ , where  $n^0$  and  $n$  were the initial and final numbers of the moles, respectively); (ii) the empiric rate constant of ethylbenzene formation  $k_{EB}$ , which was acquired by a non-linear fitting of the dependence  $a_{EB}$  on  $W/F_{BT}$  using the equation  $a_{EB} = 1 - \exp(-k_{EB} W/F_{BT})$ ; and (iii) a selectivity index  $a_{EB}/a_{DHBT}$  at  $a_{BT} = 0.5$ , which was taken from a graph of the fitting of the dependence of  $a_{BT}$ ,  $a_{EB}$  and  $a_{DHBT}$  on  $W/F_{BT}$  by four pseudo-first-order constant reaction schemes (BT to DHBT, DHBT to BT, DHBT to EB, and BT to EB).

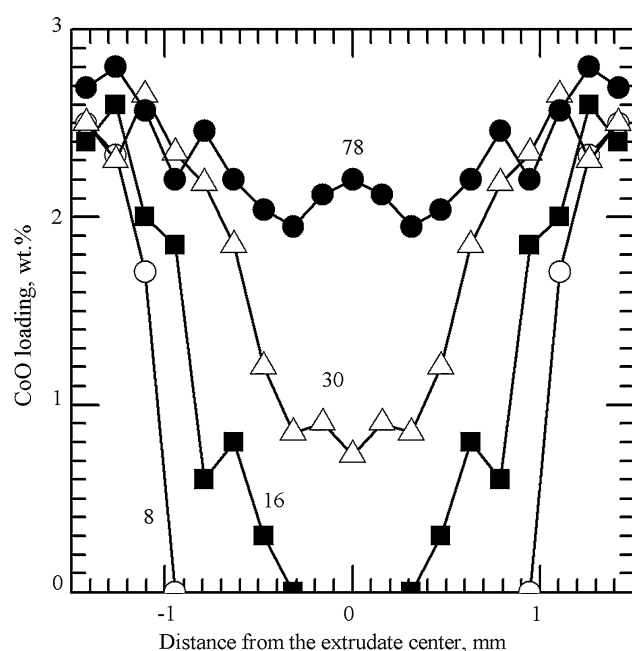
The impregnation of 20.8MoO<sub>3</sub>/ZrO(OH)<sub>2</sub> extrudates from the CoCO<sub>3</sub>/H<sub>2</sub>O slurry was monitored by EPMA (see Fig. 4 for the results). It was found that Co was being adsorbed in the form of eggshell profiles from the beginning of impregnation and an almost uniform concentration profile was achieved after 78 h. The impregnation of 7.6MoO<sub>3</sub>/ZrO<sub>2</sub> extrudates by the CoCO<sub>3</sub>/H<sub>2</sub>O slurry was not performed for two reasons: (i) we had found earlier [37] for Al<sub>2</sub>O<sub>3</sub> of the surface area 282 m<sup>2</sup>g<sup>-1</sup> that the deposition from the slurry was about 20-fold slower in the case of CoCO<sub>3</sub> than in the case of MoO<sub>3</sub> and (ii) the saturation of the ZrO<sub>2</sub> extrudates with MoO<sub>3</sub> had already took



unreacted slurry of  $\text{MoO}_3$  was removed by washing in water at the time given. **b** slurry impregnation with nominal loading being lower than the saturated adsorption loading; all  $\text{MoO}_3$  had been adsorbed at the time given. Black— $\text{MoS}_2$ , white-shadow—unloaded supports



**Fig. 3** The dependence of saturated adsorption loadings of MoO<sub>3</sub> (solid line and filled symbols) and impregnation time needed for the saturation (dashed line and open symbols) on the surface areas  $S_{\text{BET}}$  of the supports: squares—ZrO<sub>2</sub> and ZrO(OH)<sub>2</sub>, circles—TiO<sub>2</sub> [27], and triangles—Al<sub>2</sub>O<sub>3</sub> [26]. The numbers denote the external diameters in mm of the extrudates or balls studied



**Fig. 4** CoO concentration profiles evaluated by electron probe microanalysis in CoMo/ZrO(OH)<sub>2</sub> extrudates prepared by impregnation of 20.8MoO<sub>3</sub>/ZrO(OH)<sub>2</sub> from an aqueous slurry of CoCO<sub>3</sub> at 95 °C. The numbers denote impregnation times in hours

75 h because of its low surface area (see Fig. 3). The slurry impregnation of 7.6MoO<sub>3</sub>/ZrO<sub>2</sub> with CoCO<sub>3</sub> would thus take impractically long.

Due to the long time needed to saturate the extrudates, the 7.6MoO<sub>3</sub>/ZrO<sub>2</sub> catalyst and its TiO<sub>2</sub>-supported

counterpart were impregnated only in the form of grains. The adsorption loadings achieved after a 12-h reaction are included in the name of the catalysts in wt.% of CoO and are summarized in Table 1 and 2.

Despite the extremely low solubility of CoCO<sub>3</sub> in water, namely ca 0.0001 g per 100 mL at 25 °C [38], and the rather slow adsorption, the experiments clearly showed the feasibility of the slurry impregnation method application for the deposition of the compound onto supports loaded with a saturated MoO<sub>3</sub> adsorption monolayer, which could be explained by the low PZCs of the catalysts containing a saturated MoO<sub>3</sub> monolayer. The PZCs of 7.6MoO<sub>3</sub>/ZrO<sub>2</sub>, 20.8MoO<sub>3</sub>/ZrO(OH)<sub>2</sub> and 10.5MoO<sub>3</sub>/TiO<sub>2</sub> were found to be 2.4, 2.6 and 2.3, respectively (determined by the simplified mass titration method), and 2.5, 2.8, and 2.0, respectively (taken from Fig. 1). These values do not differ much from the value 2.1 (determined by the simplified mass titration method) of pure MoO<sub>3</sub>, and thus the surfaces of the prepared catalysts could be assumed to have been mostly covered by MoO<sub>3</sub>. This has already been assumed in the literature about monolayer MoO<sub>3</sub>/Al<sub>2</sub>O<sub>3</sub> [39], WO<sub>3</sub>/Al<sub>2</sub>O<sub>3</sub> [40], or V<sub>2</sub>O<sub>5</sub>/Al<sub>2</sub>O<sub>3</sub> [41] catalysts for example. The surfaces of the prepared MoO<sub>3</sub> monolayer catalysts were therefore negatively charged and the adsorption of dissolved Co cations from the slightly basic CoCO<sub>3</sub>/H<sub>2</sub>O slurry of pH 8.6 was favored.

To conclude, the depth of Mo (Co) eggshell can be easily regulated in two ways: either by the spreading time or by the nominal amount of MoO<sub>3</sub> (CoCO<sub>3</sub>). Bearing in mind the practical implications, the latter is the method of choice. To demonstrate its feasibility, the selected nominal loadings of MoO<sub>3</sub> were used to saturate ZrO(OH)<sub>2</sub> (see Fig. 2). All the MoO<sub>3</sub> had been adsorbed at the time given, and distinct eggshells were formed. All solid MoO<sub>3</sub> had disappeared from the slurry at the end of impregnation. In principle, the only by-product of the slurry impregnation method is distilled water because the low amount of dissolved Mo species that are present in mother liquor is deposited onto a surface during the drying process. As calcination is not needed, the catalyst may be directly inserted into a hydrodesulfurization reactor.

### 3.2 Hydrodesulfurization Activity

The activities of the prepared and industrial catalysts were evaluated on the model reaction of benzothiophene hydrodesulfurization and expressed as empiric pseudo-first-order rate constants of the ethylbenzene formation  $k_{\text{EB}}$ . The examples of how they were obtained are shown in Fig. 5. The particle size fraction (0.16–0.32 mm) of the catalysts with uniform and saturated loadings was used for the activity measurements because the laboratory apparatus enabled to test catalysts only in the form of grain. The



**Table 1** Activity of the prepared and reference catalysts in the HDS of benzothiophene

Catalysts	HDS activity normalized per					
	Mol of Mo (Co + Mo)		Catalyst weight		Catalyst volume	
	$k_{EB}$ , mol <sub>EB</sub> mol <sup>-1</sup> h <sup>-1</sup>	$A_R^a$	$k_{EB}$ , mmol <sub>EB</sub> g <sup>-1</sup> h <sup>-1</sup>	$A_R^a$	$k_{EB}$ , mmol <sub>EB</sub> cm <sup>-3</sup> h <sup>-1</sup>	$A_R^a$
Mo catalysts						
7.6MoO <sub>3</sub> /ZrO <sub>2</sub>	58	2.1	30	1.0	37	2.2
7.6MoO <sub>3</sub> /ZrO <sub>2</sub> (CIM)	51	1.9	27	0.9	33	1.9
10.5MoO <sub>3</sub> /TiO <sub>2</sub>	54	2.0	40	1.4	35	2.0
10.5MoO <sub>3</sub> /TiO <sub>2</sub> (CIM)	53	2.0	39	1.3	34	2.0
15MoO <sub>3</sub> /Al <sub>2</sub> O <sub>3</sub> (BASF)	27	1.0	29	1.0	17	1.0
CoMo catalysts						
1.7CoO6.4MoO <sub>3</sub> /ZrO <sub>2</sub>	182	0.6	122	0.3	149	0.5
2.0CoO(CIM)7.4MoO <sub>3</sub> /ZrO <sub>2</sub>	107	0.4	96	0.2	121	0.4
1.7CoO(MIM)8.2MoS <sub>2</sub> /ZrO <sub>2</sub>	250	0.9	188	0.4	238	0.8
2.6CoO10.0MoO <sub>3</sub> /TiO <sub>2</sub>	157	0.6	163	0.4	147	0.5
2.4CoO(CIM)11.5MoO <sub>3</sub> /TiO <sub>2</sub>	142	0.5	159	0.4	146	0.5
3.2CoO(MIM)11.1MoS <sub>2</sub> /TiO <sub>2</sub>	176	0.6	197	0.5	181	0.6
3.2CoO15.5MoO <sub>3</sub> /Al <sub>2</sub> O <sub>3</sub> (KF)	282	1.0	421	1.0	300	1.0

<sup>a</sup>  $A_R$ —relative activity**Table 2** Promotional effect of Co on the HDS activity of the Mo catalysts prepared

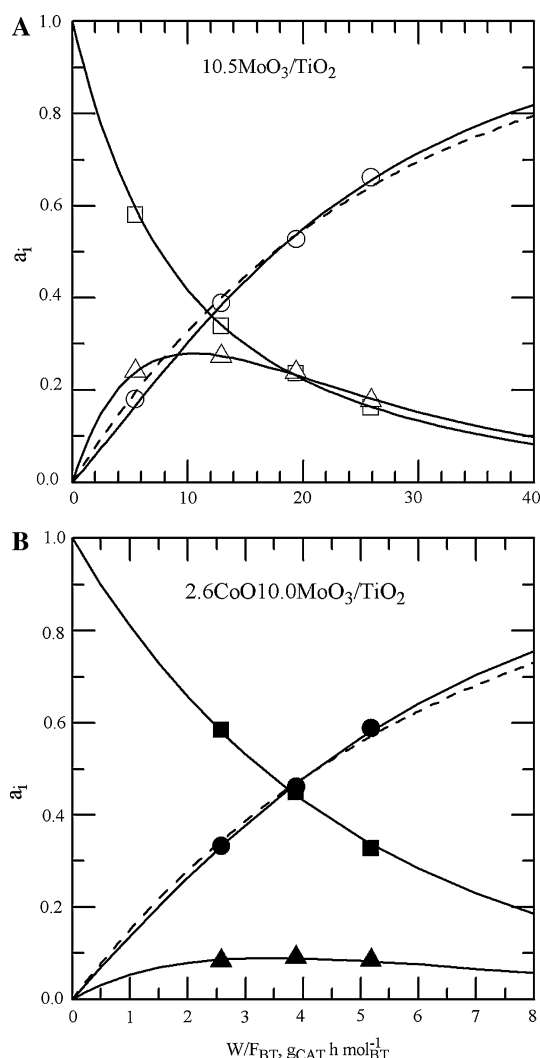
Catalyst	Molar ratio (Co/Co + Mo)	Promotional effect of Co ( $k_{EB}^{CoMo}/k_{EB}^{Mo}$ ) normalized per		
		Mol of Co + Mo	Catalyst weight	Catalyst volume
1.7CoO6.4MoO <sub>3</sub> /ZrO <sub>2</sub>	0.34	3.1	4.1	4.0
2.0CoO(CIM)7.4MoO <sub>3</sub> /ZrO <sub>2</sub>	0.29	1.8	3.2	3.3
1.7CoO(MIM)8.2MoS <sub>2</sub> /ZrO <sub>2</sub>	0.31	4.3	6.3	6.4
2.6CoO10.0MoO <sub>3</sub> /TiO <sub>2</sub>	0.33	2.9	4.1	4.2
2.4CoO(CIM)11.5MoO <sub>3</sub> /TiO <sub>2</sub>	0.29	2.6	4.0	4.2
3.2CoO(MIM)11.1MoS <sub>2</sub> /TiO <sub>2</sub>	0.38	3.3	4.9	5.2

activities were normalized per number of mol of the active metals or per unit weight or volume of the catalyst. The normalization per mol of the active metals makes it possible to compare the activities of the catalysts with different loadings (as it was shown in Fig. 3, the saturated adsorption loadings depended on the surface areas of the ZrO<sub>2</sub> and TiO<sub>2</sub> supports). This activity is an intrinsic property of the sulfided transition metal and its interaction with the support. On the contrary, the activity normalized per unit weight or volume represent an integral value of HDS activity. The normalization per unit volume was calculated using the determined packing density of 1.14, 0.79, 0.60 and 0.71 gcm<sup>-3</sup> of the ZrO<sub>2</sub>, TiO<sub>2</sub>, Mo/Al<sub>2</sub>O<sub>3</sub> BASF and CoMo/Al<sub>2</sub>O<sub>3</sub> KF 756, respectively. The volume based activity provides a basis of comparison for commercial HDS processes as the reactor volume is generally fixed in existing facilities. For the sake of clarity, the relative activities of the prepared catalysts  $A_R$  were calculated as the ratio of the  $k_{EB}$  of the prepared catalyst to the  $k_{EB}$  of

the industrial reference counterpart. An overview of the HDS activities is shown in Table 1, which, however, does not contain data on the ZrO(OH)<sub>2</sub>-supported catalysts, because we have previously found that they exhibited extremely low HDS activity, (see [17] for further details).

It was ascertained that the intrinsic activity of the Mo deposited by the slurry impregnation method was slightly higher than the activity of the Mo deposited by conventional impregnation from an aqueous (NH<sub>4</sub>)<sub>6</sub>Mo<sub>7</sub>O<sub>24</sub> solution. The Mo deposited over ZrO<sub>2</sub> and TiO<sub>2</sub> was, moreover, approximately twice as active as the Mo deposited over Al<sub>2</sub>O<sub>3</sub> in the industrial reference catalyst. After normalization, the ZrO<sub>2</sub>- and TiO<sub>2</sub>-supported Mo catalysts retained their high activity per unit volume while losing their advantage per unit weight due to the relatively higher packing density of ZrO<sub>2</sub> and TiO<sub>2</sub> to the Mo/Al<sub>2</sub>O<sub>3</sub>.

Furthermore, the impregnation method using the CoCO<sub>3</sub>/H<sub>2</sub>O slurry was found to be efficient for the enhancement of the HDS activity of the ZrO<sub>2</sub>- and TiO<sub>2</sub>-

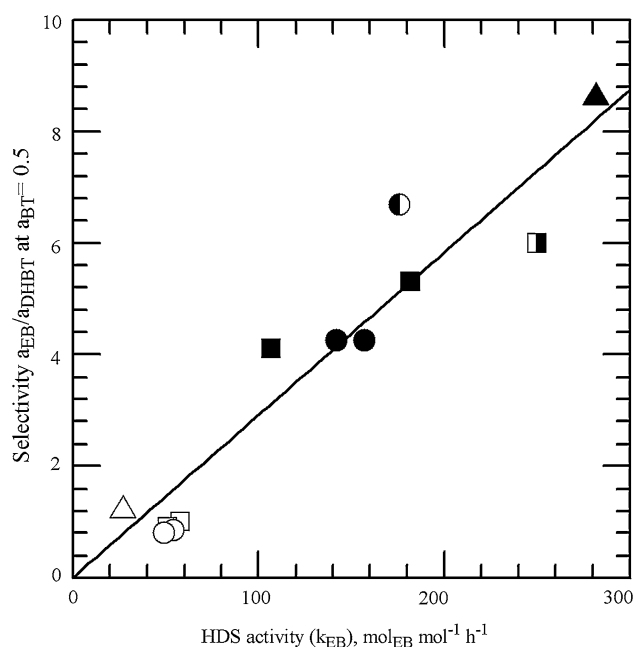


**Fig. 5** Examples of the kinetic curves of benzothiophene HDS. Squares—benzothiophene, triangles—dihydrobenzothiophene, and circles—ethylbenzene. The solid and dashed curves have been calculated using the four pseudo-first-order reaction schemes and the empiric pseudo-first-order equation of ethylbenzene formation, respectively

supported  $\text{MoO}_3$  catalysts. The promotional effect of Co on HDS activity was quantified as a ratio of the formal-rate constant determined over a CoMo catalyst to the formal-rate constant determined over a corresponding Mo counterpart ( $k_{\text{EB}}^{\text{CoMo}}/k_{\text{EB}}^{\text{Mo}}$ ). The promotional effects are summarized in Table 2.

It was ascertained that the methods of Co deposition over  $\text{ZrO}_2$ - and  $\text{TiO}_2$ -supported  $\text{MoO}_3$  catalysts may be ordered on the basis of the resulting HDS activity and the promotional effects as follows: the conventional deposition from an aqueous  $\text{Co}(\text{NO}_3)_2$  solution < the slurry impregnation with  $\text{CoCO}_3$  < the deposition from a methanolic  $\text{Co}(\text{C}_5\text{H}_7\text{O}_2)_2$  solution onto a pre-sulfided Mo catalyst.

As the promotional effect of Co on the activity in the HDS of benzothiophene was observed to be accompanied



**Fig. 6** The dependence of the selectivity index on HDS activity over the prepared and reference catalysts. The squares, circles and triangles were used for the  $\text{ZrO}_2$ -,  $\text{TiO}_2$ - and reference industrial  $\text{Al}_2\text{O}_3$ -supported catalysts, respectively. Open symbols—Mo catalysts, filled symbols—CoMo catalysts with Co deposited by SIM or CIM, half-filled symbols—CoMo catalysts with Co deposited by MIM over presulfided Mo catalysts

by a relative increase of C–S hydrogenolysis (HYG) to C=C hydrogenation (HYD), which was manifested by a decrease of the formation of hydrogenation intermediate dihydrobenzothiophene, a selectivity index  $a_{\text{EB}}/a_{\text{DHBT}}$  was calculated as a ratio of the relative composition of ethylbenzene to the relative composition of dihydrobenzothiophene at the relative composition of benzothiophene 0.5. The promotional effect and selectivity index were plotted against the HDS activity in Fig. 6. First, it was found that the  $a_{\text{EB}}/a_{\text{DHBT}}$  selectivity increased roughly linearly with the increasing HDS activity. Second, the  $\text{ZrO}_2$  and  $\text{TiO}_2$  supports hardly influenced the relative selectivity  $a_{\text{EB}}/a_{\text{DHBT}}$  of the deposited Mo while the intrinsic HDS activity of that Mo was two times higher than was achieved over the reference  $\text{Al}_2\text{O}_3$ -supported Mo catalyst. The CoMo catalysts supported over  $\text{ZrO}_2$  and  $\text{TiO}_2$  supports, however, exhibited lower  $a_{\text{EB}}/a_{\text{DHBT}}$  selectivities and HDS activities than the reference catalyst CoMo supported over  $\text{Al}_2\text{O}_3$ . The effect of the  $\text{ZrO}_2$  and  $\text{TiO}_2$  supports may therefore be considered as detrimental to the activity of the bimetallic CoMo phase. The most promising method of Co deposition, the promotion of the presulfided Mo by cobalt–acetylacetonate, only partially compensated for this disadvantage. These results are in good agreement with previous literature data [16, 42]. For example, the

promotional effects of 2.4 and 2.9 in the case of Co over zirconia- and titania-supported catalysts, respectively, in [42] or 3.3 over both supports in [16] were reported while they were about 5 or 11 over alumina-supported counterparts resulting in high integral HDS activity. On contrary, it is believed that further improvement of the ZrO<sub>2</sub> and TiO<sub>2</sub> based catalysts lie in tailored preparation of their mixed form with desirable textural properties [43–45] or nanostructured forms [46, 47]. The CoMo catalyst supported on solvo-thermally treated ZrO<sub>2</sub>–TiO<sub>2</sub> with molar ratio ZrO<sub>2</sub>/TiO<sub>2</sub> 30/70 and BET surface area 313 m<sup>2</sup>g<sup>−1</sup> exhibited promotional effect about 3.2 but exceeded the HDS activity of a reference Al<sub>2</sub>O<sub>3</sub>-supported counterpart about twofold [43]. The promotional effect of 8.5 was reached after deposition of Co onto presulfided Mo catalysts supported on ZrO<sub>2</sub>–TiO<sub>2</sub> with molar ratio ZrO<sub>2</sub>/TiO<sub>2</sub> 60/40 and BET surface area 165 m<sup>2</sup>g<sup>−1</sup>, which resulted in 10% activity improvement in comparison with Al<sub>2</sub>O<sub>3</sub> supported catalyst [44]. Two fold higher HDS activities of CoMo catalysts were reported over nano-structured TiO<sub>2</sub> possessing BET surface area about 330 m<sup>2</sup>g<sup>−1</sup> [46] and TiO<sub>2</sub> nanotubes of BET surface area 236 m<sup>2</sup>g<sup>−1</sup> [47] than over Al<sub>2</sub>O<sub>3</sub>-supported counterparts but without referring on promotional effects. A relatively high promotional effect of 10 was obtained in the case of Ni supported over wide-pore ZrO<sub>2</sub>–TiO<sub>2</sub> Mo catalyst (molar ratio ZrO<sub>2</sub>/TiO<sub>2</sub> 30/70 and BET surface area about 300 m<sup>2</sup>g<sup>−1</sup>) employing chelating agent assisted impregnation technique [45]. It could be assumed that applying the same preparation technique to the ZrO<sub>2</sub> support studied within the present work could led to further improvement of the HDS activity.

#### 4 Conclusions

It has been shown that the slurry impregnation method is suitable for the deposition of MoO<sub>3</sub> onto the extrudates of ZrO<sub>2</sub> and ZrO(OH)<sub>2</sub> in order to form an eggshell radial profile of Mo concentration. This method, moreover, does not make it possible to exceed the dispersion capacity of the support surface. The thickness of the eggshell can be efficiently regulated by the amount of MoO<sub>3</sub> used. Co can be deposited over the ZrO<sub>2</sub>- and TiO<sub>2</sub>-supported catalysts containing a saturated adsorption monolayer of MoO<sub>3</sub> from an aqueous slurry of low solubility CoCO<sub>3</sub>. The slurry impregnation method is a clean and simple method of Co and Mo deposition, which does not introduce any ions like NH<sub>4</sub><sup>(+)</sup> or NO<sub>3</sub><sup>(−)</sup>; furthermore, calcination is not needed, and only water is produced during drying. The activity of the Mo supported on ZrO<sub>2</sub> and TiO<sub>2</sub> in the hydrodesulfurization of

benzothiophene was about twice as high as the activity of the Mo in the industrial Al<sub>2</sub>O<sub>3</sub>-supported catalyst. The activity of CoMo ZrO<sub>2</sub>- and TiO<sub>2</sub>-supported catalysts, however, was not as high as the activity of the industrial, Al<sub>2</sub>O<sub>3</sub>-supported counterpart.

**Acknowledgment** The financial support of the Grant Agency of the Czech Republic is gratefully acknowledged (Grants No. 104/06/P034 and 104/06/0705).

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